

REPORT ON
SOIL INVESTIGATION FOR CONSTRUCTION OF SHIKSHA
BHAWAN (G+4) AT MADHEPURA.

Submitted to

CHIEF ENGINEER
BSEIDC, PATNA

SHAMVWI CONSULTANT
414, Jagat Trade Centre,
Fraser Road, Patna – 800001
Tel.: 0612 – 2950329, 2366308,
Mobile: +919835218184,8986215718.

PREFACE

The present report on sub-soil investigation was carried out as per Chief Engineer, BSEIDC, Patna letter no BSEIDC/TECH/1960(P)/2018-3609 dated 21.04.2023.

The entire investigation process was broadly divided into two category –one field work and second was laboratory work.

Field work includes conducting SPT ,Dynamic cone test, collection of disturbed as well as undisturbed soil samples from different location and different depth of sub-soil strata.

It was tried to get information from local people to get an idea about variation of water table during different season of year and also to get first hand information about type of foundation usually provided in the locality.

We thanks Prof. M.P.Jakhanwal(Retired) ,M.Tech ,Ph.D. ,Muzaffarpur Institute of Technology, Muzaffarpur for his valuable advice during laboratory test and during preparation of report.

Client's help is gratefully acknowledged in providing Bore hole locations, cooperation and guidance during finalization of report.

We belief that the present report will serve the purpose, for which sub-soil investigation has been carried out.

Anil Kumar Sariar

ANIL KUMAR SARIAR
Partner, Shamvvi Consultant

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REPORT ON SUB-SOIL INVESTIGATION FOR THE CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA.

1. INTRODUCTION

The objective of subsoil investigation reported here in, were taken up, to find out the nature of subsoil at the site of the proposed construction and to recommend the type or types of foundation suitable for it and the corresponding allowable bearing capacity.

The necessary field tests were carried out at the site. Soil samples from various depths in the different bore holes were collected, transported, carefully to the laboratory and tested to determine the engineering properties of the soil.

Based on the test results, certain recommendation were made and given in this report, regarding the type of foundation suitable for the proposed project and the allowable bearing capacity for certain sizes thereof.

2. TOPOGRAPHY

The land in question was even.

3. FIELD WORK

The field work consists of boring, soil sampling and conduct of Standard penetration tests and Dynamic cone penetration tests.

3.1 BORING

An appropriate number of boreholes of adequate depth were sunk at suitable spots as per direction of Engineer-in-charge. The details of the boreholes are given in table-1.

Table 1: Details of bore holes

DIAMETER OF BORE MM	DEPTH M	BORE HOLE
150	10.5	3 Bore Holes (BH-1 to BH-3)

The borings were kept dry while advancing through partially saturated soil. The position of water table in a borehole was recorded at least 48 hours after the stopping of the boring operation.

For boring below ground water level, the borehole was kept filled with water upto that level during boring.

3.2 SAMPLING

Undisturbed & disturbed samples were collected at different depth/where change of strata occurred. Identification slips were provided both inside and outside the tube.

On arrival in laboratory, the identification slips were checked against the boring and sampling records.

Samples were extracted from the tubes just before testing.

3.3 STANDARD PENETRATION TEST

This test was performed in the boreholes at interval of depth of 1.5m, or at the change of strata/ as per IS: 2131 of 1963.

3.4 DYNAMIC CONE PENETRATION TEST

This test was performed when a bore hole could not be advanced to desired depth due to caving- in of the soil, or when it was felt necessary to supplement the information gained from SPT. This test was performed, as per relevant IS code till high value of penetration resistance was encountered or till desired depth of investigation was reached, at which stage the test was stopped.

CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA.

4. LABORATORY TEST

Lab. Test was performed to determine the following properties of soil samples as per relevant I.S. code.

- (a) Natural moisture content.
- (b) Bulk density.
- (c) Atterberg's limits (on fine grained soil only)
- (d) Grain size analysis.
- (e) Specific gravity.
- (f) Shear test.
- (i) Unconfined/triaxial compression tests for fine-grained soils.
- (ii) Direct shear test for coarse-grained soils.
- (g) Consolidation tests for fine grained soils.
- (h) Organic content, chemical test etc.
- (i) pH of soil and water.
- (j) Free swell Index
- (k) Crushing strength test (uniaxial)

4.1 SAMPLE EXTRACTION & PREPARATION OF TEST SPECIMENS

Samples for different tests were prepared as per method described in relevant IS code/as per method described in standard book.

4.2 ROUTINE CLASSIFICATION TESTS.

Tests for the determination of natural moisture content, bulk density, Atterberg's limit, grain size distribution and specific gravity were performed as per IS code on representative disturbed soil samples, wherever felt necessary. The results were used in classifying the soils of different strata as per IS code 1498-1970.

5.0 PRESENTATION OF TEST RESULT

Results were presented in table form on the following pages.

6.0 METHOD FOR CALCULATION OF ALLOWABLE BEARING CAPACITY

6.1 COHESIVE SOIL

Net ultimate bearing capacity was calculated as per IS-6403-1981.
 $q_d = cN_c S_c D_c I_c$

q_d = net ultimate bearing capacity

$N_c = 5.14$

$S_c = 1$ for strip footing

$D_c = 1 + 0.2 * D/B$

$I_c = 1$ for vertical loading

c = cohesion obtained through unconfined compression test for depth of $2B/3$ below the foundation.

Settlement criteria

$S = H / (1 + e_0) * C_c * \log((p_0 + p_1) / p_0)$

S = settlement

H = thickness of compressible layer

CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA

e_o =initial void ratio

p_o =initial effective pressure

p_1 =pressure increment

C_c =compression index

6.2 Soil with the value of c & θ

Net ultimate bearing capacity was calculated as per IS 6403-1981

$$Q_d = c N_c S_c D_c I_c + q (N_q - 1) S_q D_q I_q + 0.5 R^* B N_r^* S_r^* D_r^* I_r^* w'$$

For local shear failure

$$\tan \theta' = 0.67 \tan \theta$$

$$C' = 2 * c / 3$$

$S_c = S_q = S_r = 1$ for strip footing

$$D_c = 1 + 0.2 * (D/B) * \tan(45 + \theta/2)$$

$I_c = I_q = I_r = 1$ for vertical loading

$$D_q = D_r = 1 + 0.1 * (D/B) \tan(45 + \theta/2)$$

$$q = (R - R_w) * D$$

M = moisture content

R = bulk density of soil

R_w = unit weight of water

L.L. = liquid limit

P.L. = plastic limit

S.L. = shrinkage limit

D = depth below ground level

Settlement criteria

The net allowable bearing capacity for a permissible settlement of 25mm, was obtained by

teng's formula

$$Q_{na} = 3.5 * (N-3) * \{(B+0.3)/2 * B\} * \{(B+0.3)/2 * B\} * w' * F_d$$

N = corrected N

$F_d = 1 + D/B$ less than or equal to 2

CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA

7.0 METHOD FOR CALCULATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part I/Sec 2-1979

7.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

$$Q = A_p \cdot N_c \cdot C_p + a \cdot C \cdot A_s$$

A_p = cross sectional area of pile toe in cm²

N_c = Bearing capacity factor usually taken as 9

C_p = average cohesion at pile tip in Kg/cm

a = reduction factor

C = average cohesion throughout the length of pile in kg/cm²

A_s = surface area of pile shaft in cm²

8.0 METHOD FOR CALCULATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part III-1980

8.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

$$Q = A_p \cdot N_c \cdot C_p + A_a \cdot N_c \cdot C'_a + C'_a \cdot A_s' + \alpha \cdot C_a \cdot A_s$$

A_p = cross sectional area of pile toe in cm²

N_c = Bearing capacity factor usually taken as 9

C_p = cohesion of soil around toe.

α = reduction factor

$$A_a = \pi \cdot (D_u^2 - D^2) / 4$$

C'_a = average cohesion around under ream

D_u = dia of under-ream, D = dia of pile

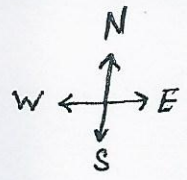
A_s' = surface area of pile shaft in cm²

A_s = surface area of stem

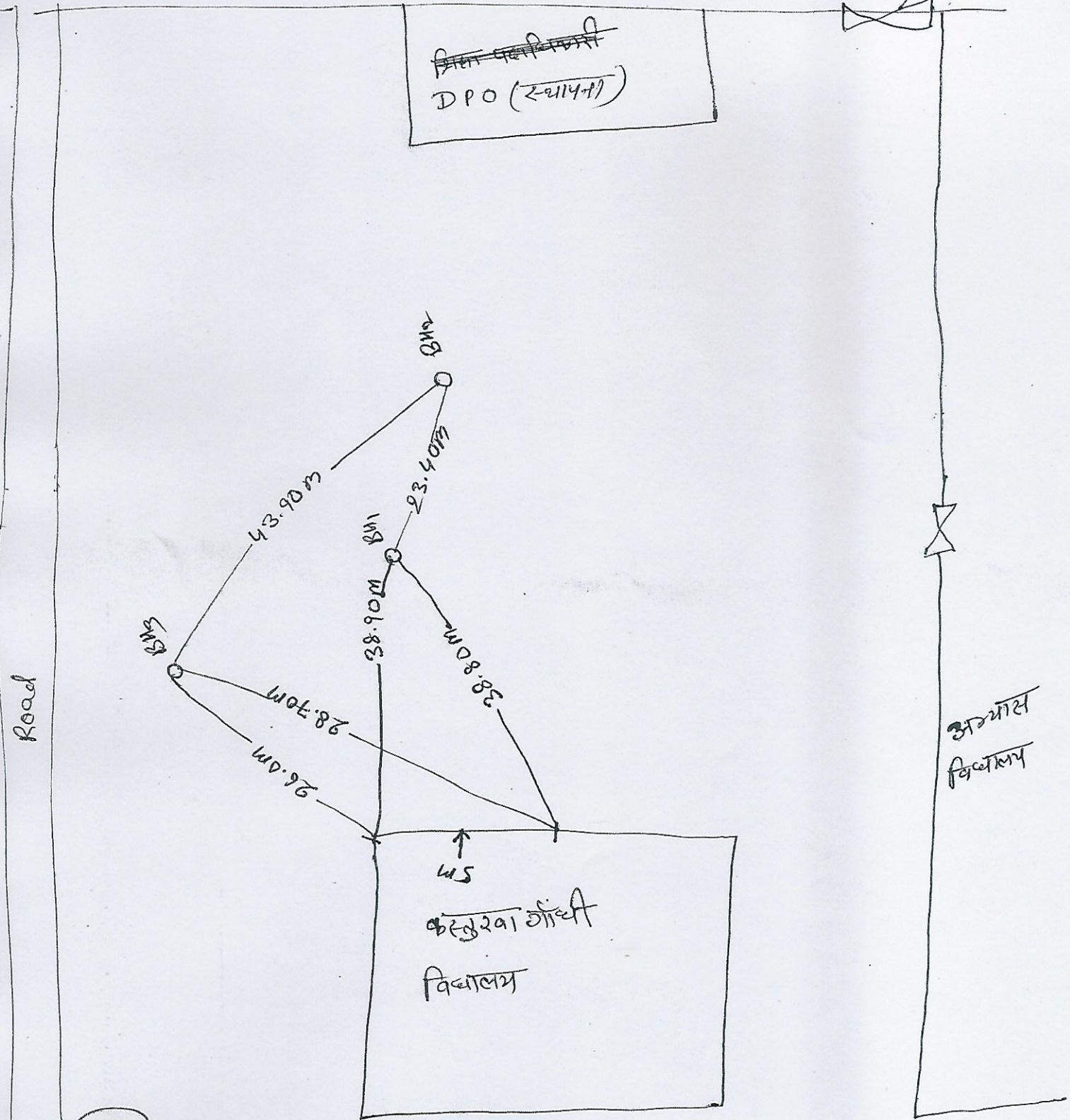
A_s' = surface area of the cylinder circumscribing the under ream.

SIKSHA BHAWAN MADHEPURA

SIKSHA BHAWAN AT MADHEPURA



R O A D



Rajesh
24/05/2023
J-5 055106
Bolu Dr.



SAMPLE NO	DEPTH OF SAMPLE	OBSERVED VALUE	CORRECTED VALUE	STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.I.S CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	TYPE OF TEST	SHEAR TEST				UNCONFINED COMPRESSION TEST q_c (kg/cm ²)	COEFFICIENT OF VOLUME COMPRESSION M_v (cm ³ /kg)	TABLE NO : 3	
				5	10	20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)				GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)				COHESION c (kg/cm ²)
DS5																											
SPT5	7.5	26					0.0	98.40	1.6			NON-PLASTIC			1.96	1.73	13.4	2.68	DST	0	30.00						
DS6																											
SPT6	9.0	26					0.0	97.40	2.6			NON-PLASTIC			1.96	1.73	13.1	2.68									
DS7																											
SPT7	10.5	37					0.9	97.50	1.6			NON-PLASTIC			1.96	1.72	13.8	2.68	DST	0	30.00						
DS8																											
SPT8	12.0	46					0.0	98.60	1.4			NON-PLASTIC			1.96	1.72	13.8	2.68									
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST				UCT : UNCONFINED COMPRESSION SHEAR TEST														DST : DIRECT SHEAR TEST									
! SAMPLE SLIPPED ~ TEST ON REMOULDED SAMPLE				UDS : UNDISTURBED SAMPLE														SPT : STANDARD PENETRATION TEST VALUE									
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																											

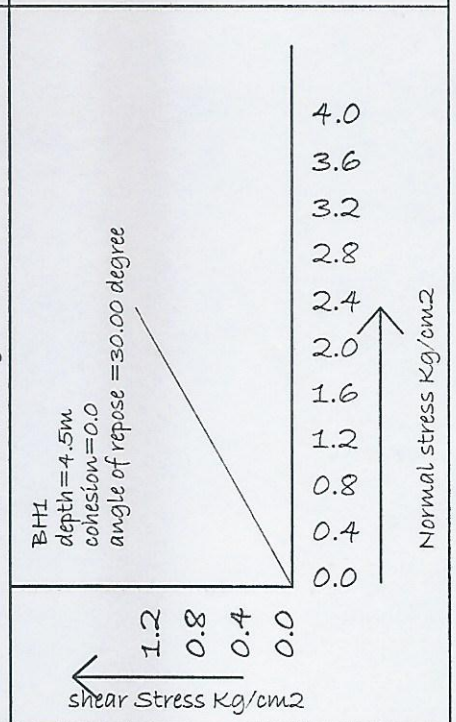
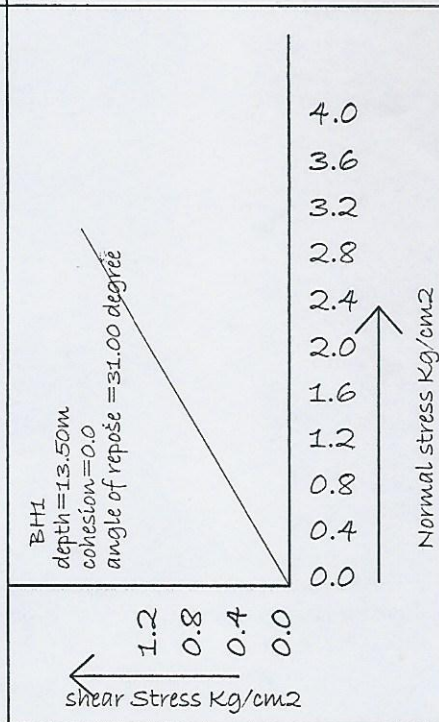
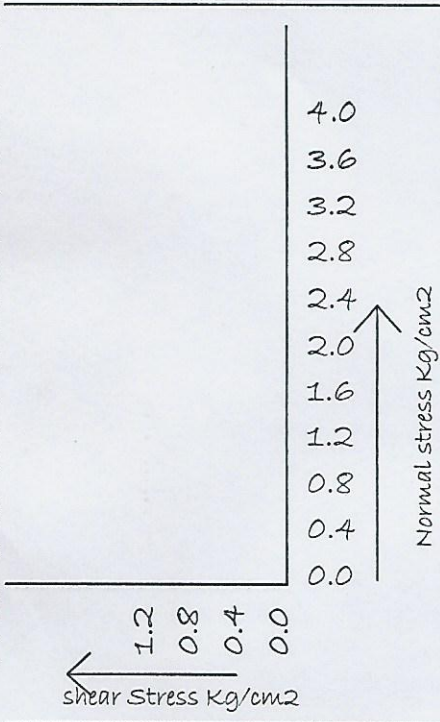
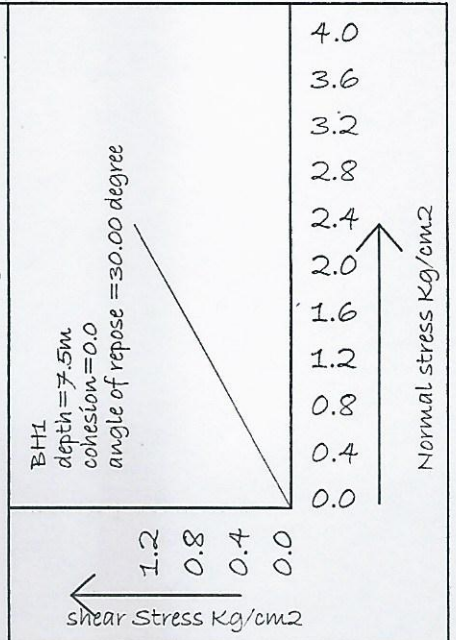
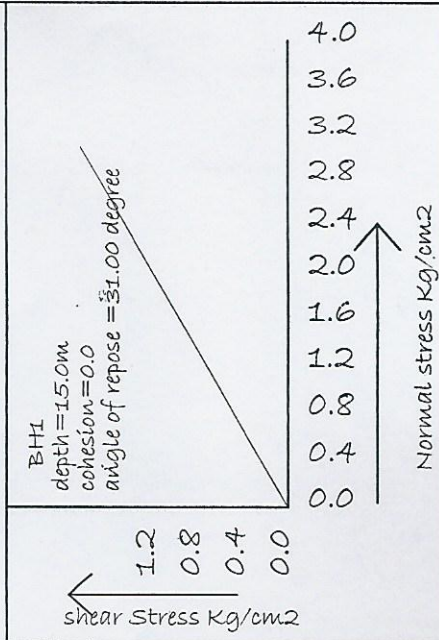
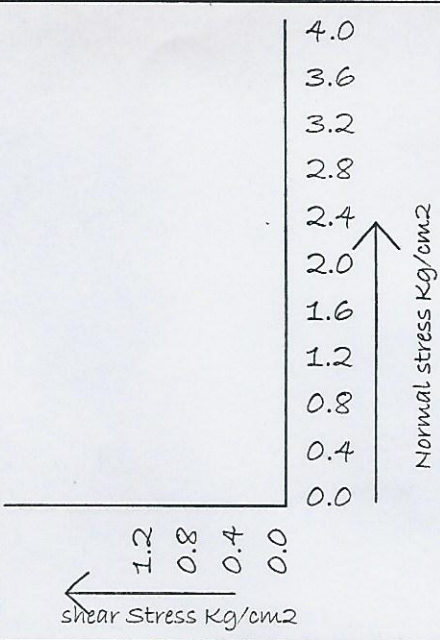
SHAMAWI CONSULTANTS 414J.T.C., FRASE R ROAD, PATNA		NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA										BORING DATES START : 20.05.2004 FINISH : 21.05.2004		TERMINATION DEPTH : 15 WATER TABLE DEPTH : 1.9		TABLE NO : 7 BORE HOLE NO : BH1											
SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				CONSISTENCY LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)		SPECIFIC GRAVITY		SHEAR TEST		CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST, q_u kg/cm ²	COEFFICIENT OF VOLUME COMPRESSIONITY M_v cm ³ /kg	
		OBSERVED VALUE	CORRECTED VALUE	GRAVEL (%)	SAND (%)	SILT (%)		CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	SHRINKAGE LIMIT	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	NATURAL MOISTURE CONTENT (%)	TYPE OF TEST	COHESION c (kg/cm ²)	ANGLE OF FRICTION IN DEGREE	VOID RATIO e_o	COMPRESSION INDEX C_c								
DS9																											
SPT9	13.5	43			98.60	1.4		NON-PLASTIC				1.96	1.74	12.5	2.68	DST	0	31.00									
DS10																											
SPT10	15.0	41			98.40	1.6		NON-PLASTIC				1.96	1.74	12.5	2.68	DST	0	31.00									
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST		UCT : UNCONFINED COMPRESSION SHEAR TEST										DST : DIRECT SHEAR TEST															
I SAMPLE SLIPED ~ TEST ON REMOULDED SAMPLE		UDS : UNDISTURBED SAMPLE										SPT : STANDARD PENETRATION TEST VALUE															
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																											

SHAMVVI CONSULTANTS 414J.T.C.FRASE R ROAD, PATNA		NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA															BORING DATES START :26.05.2023 FINISH :27.05.2023		TERMINATION DEPTH :15.0m WATER TABLE DEPTH : 4.2M		TABLE NO :8 BORE HOLE NO :BH3								
SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)		SPECIFIC GRAVITY		TYPE OF TEST	COHESION c (kg/cm ²)	ANGLE OF FRICTION IN DEGREE	CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST _{qu} (kg/cm ²)	COEFFICIENT OF VOLUME COMPRESSIBILITY M _v (cm ³ /kg)		
		OBSERVED VALUE	CORRECTED VALUE	5	10	20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	VOID RATIO e _o	COMPRESSION INDEX C _c											
DS	G.L.																												
DS1																													
SPT1	1.5	13					SAND SP	0.0	90.50	9.5		NON-PLASTIC	1.94	1.74	11.2	2.70					DST	0	29.0						
DS2																													
SPT2	3	15					SAND SP	0.0	90.20	9.8		NON-PLASTIC	1.94	1.74	11.5	2.70													
DS3																													
SPT3	4.5	10					SAND SP	0.0	90.50	9.5		NON-PLASTIC	1.94	1.74	11.5	2.70					DST	0	30.00						
DS4																													
SPT4	6	24					SAND SP	0.0	98.30	1.7		NON-PLASTIC	1.94	1.74	11.8	2.68													
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST		UCT : UNCONFINED COMPRESSION SHEAR TEST DST : DIRECT SHEAR TEST																											
I SAMPLE SLIPPED ~ TEST ON REMOULDED SAMPLE		UDS : UNDISTURBED SAMPLE															SPT : STANDARD PENETRATION TEST VALUE												
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																													

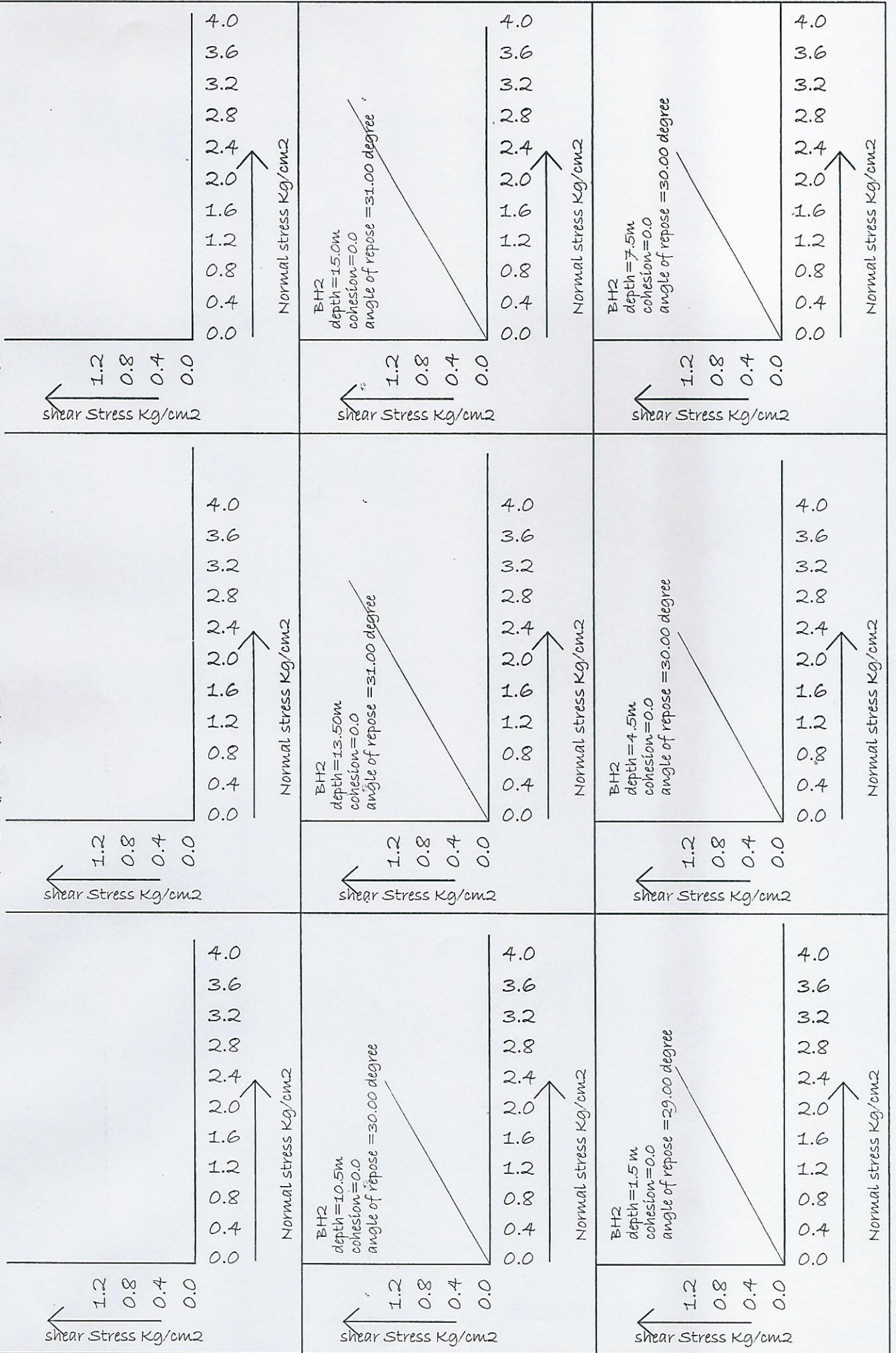
SHAMWVI CONSULTANTS 414J.T.C., FRASE R ROAD, PATNA		NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA										BORING DATES DEPTH : 15.0m		TERMINATION DEPTH : 15.0m		TABLE NO : 9														
SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)		SPECIFIC GRAVITY		SHEAR TEST		CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST q_u kg/cm ²	COEFFICIENT OF VOLUME COMPRESSION M_v cm ³ /kg				
		OBSERVED VALUE	CORRECTED VALUE	5	10	20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	NATURAL MOISTURE CONTENT (%)	GRAVITY	TYPE OF TEST	COHESION c (kg/cm ²)	ANGLE OF FRICTION IN DEGREE	VOID RATIO e_o	COMPRESSION INDEX C_c							
DS5							SAND SP	0.0	98.50	1.5						1.96	1.74	12.5	2.68											
SPT5	7.5	27					SAND SP	0.0	97.80	2.2						1.96	1.74	12.8	2.68											
DS6							SAND SP	0.0	97.80	1.3						1.96	1.73	13.6	2.68											
SPT6	9.0	25					SAND SP	0.9	97.80	1.3						1.96	1.72	13.7	2.68											
DS7							SAND SP	0.0	99.10	0.9						1.96	1.72	13.7	2.68											
SPT7	10.5	37					SAND SP	0.0	99.10	0.9						1.96	1.72	13.7	2.68											
DS8							SAND SP	0.0	99.10	0.9						1.96	1.72	13.7	2.68											
SPT8	12.0	40					SAND SP	0.0	99.10	0.9						1.96	1.72	13.7	2.68											
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST							UCT : UNCONFINED COMPRESSION SHEAR TEST								DST : DIRECT SHEAR TEST															
! SAMPLE SLIPPED ~ TEST ON REMOULDED SAMPLE							UDS : UNDISTURBED SAMPLE								SPT : STANDARD PENETRATION TEST VALUE															
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																														

SHAMVVI CONSULTANTS 414J.T.C., FRASE R ROAD, PATNA		NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA										BORING DATES : TERMINATION DEPTH : 15 WATER TABLE DEPTH : 1.9			TABLE NO : 10																					
SAMPLE NO	DEPTH OF SAMPLE	OBSERVED VALUE	CORRECTED VALUE	STANDARD PENETRATION RESISTANCE CURVE		VISUAL DESCRIPTION OF SOIL WITH B.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				CONSISTENCY LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST					UNCONFINED COMPRESSION TEST q _u (kg/cm ²)	COEFFICIENT OF VOLUME COMPRESSIONIBILITY M _v												
				SPT BLOWS PER 30 CM	5		10	20	GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	SHRINKAGE LIMIT			BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	VOID RATIO e ₀	COMPRESSION INDEX C _c	TYPE OF TEST			COHESION c (kg/cm ²)	ANGLE OF FRICTION IN DEGREE										
DS9																																				
SPT9	13.5	40				SAND SP	0.0	99.10	0.9		NON-PLASTIC	1.96	1.73	13.4	2.68																					
DS10																																				
SPT10	15.0	37				SAND SP	0.0	98.80	1.2		NON-PLASTIC	1.96	1.73	13.4	2.68																					
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST				UCT : UNCONFINED COMPRESSION SHEAR TEST														DST : DIRECT SHEAR TEST																		
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NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																																				

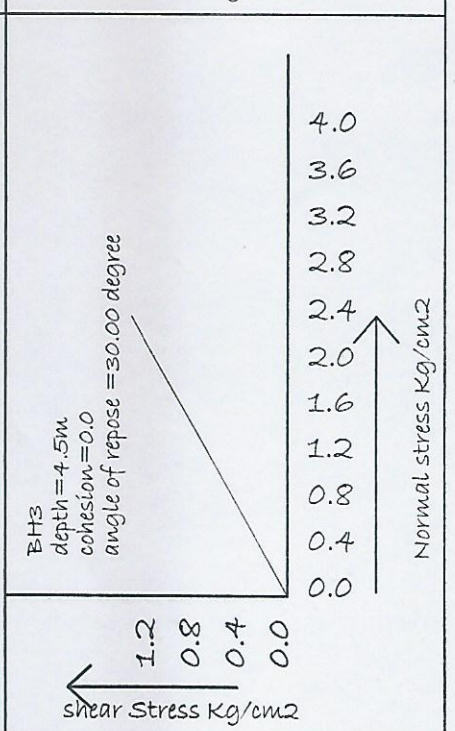
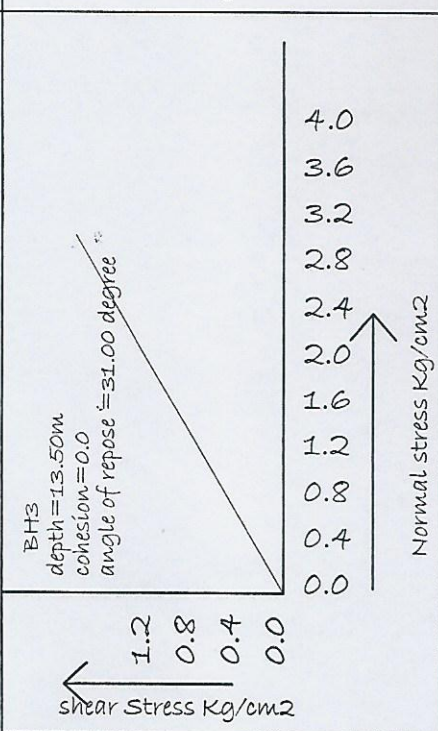
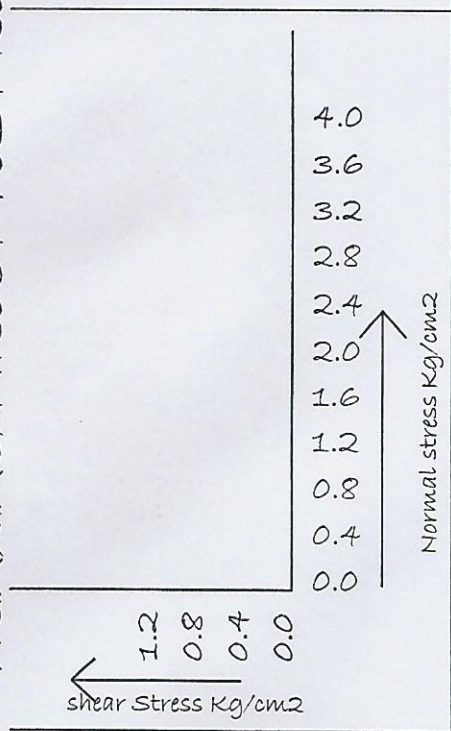
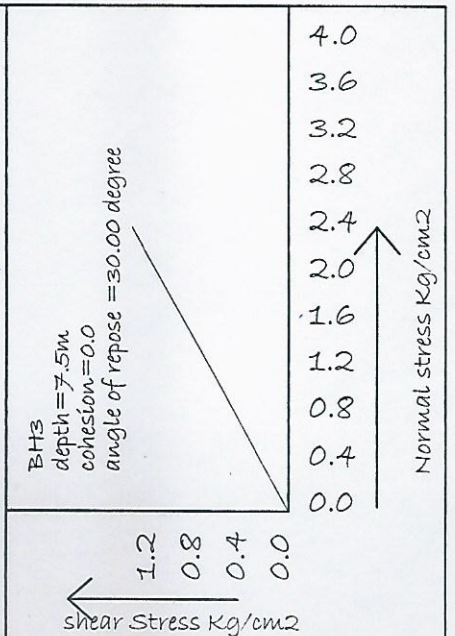
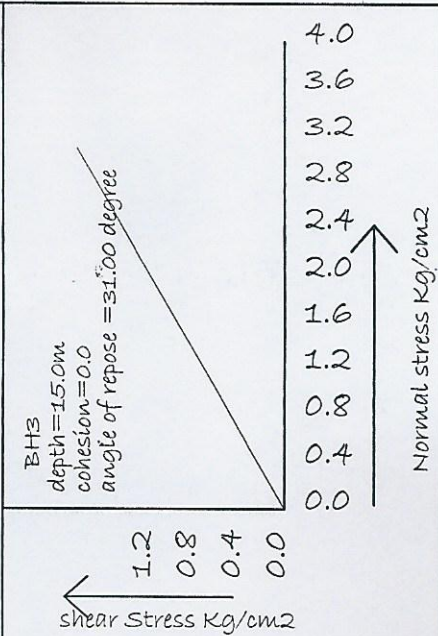
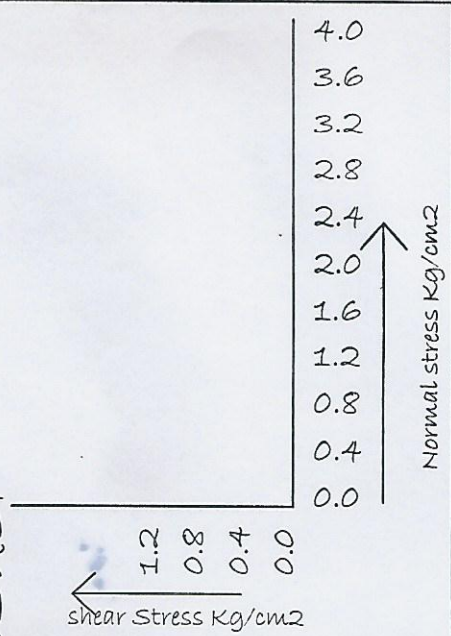
TRIAxIAL/DIRECT TEST RESULT



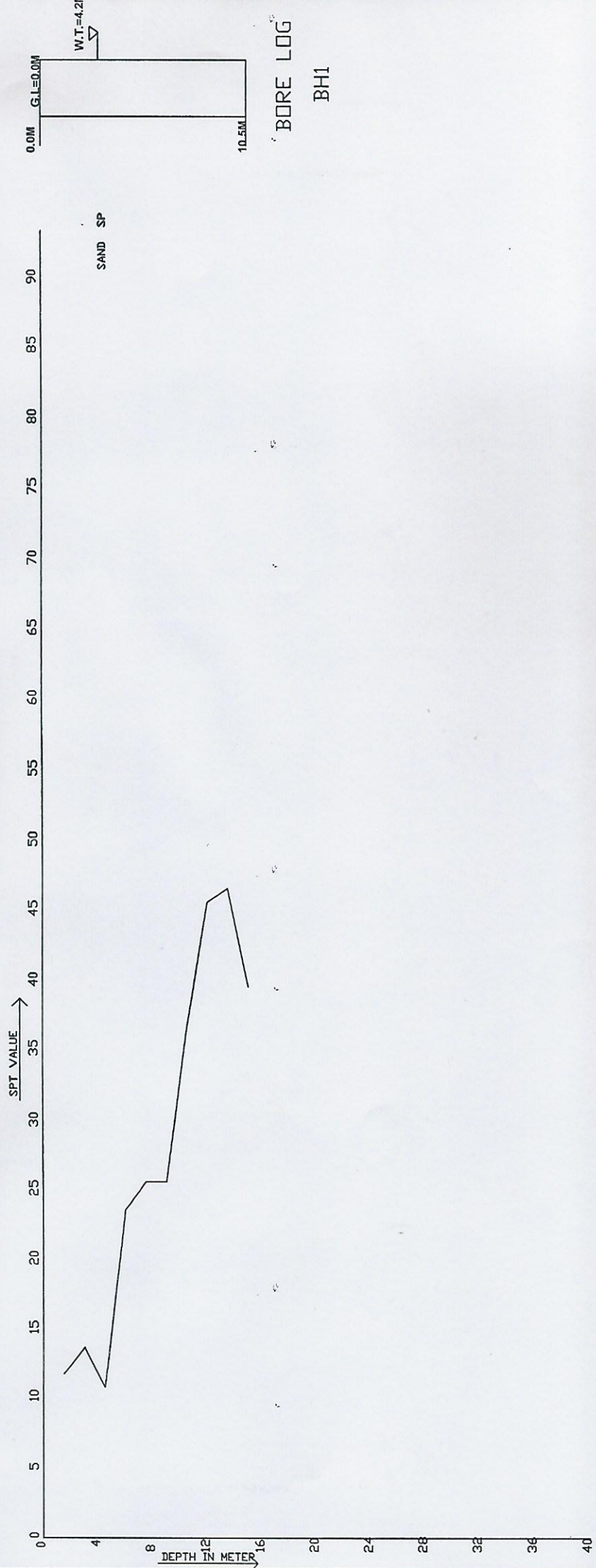
TRIAxIAL/DIRECT TEST RESULT



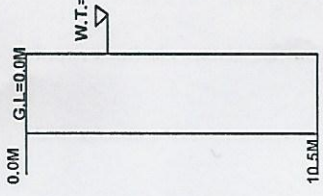
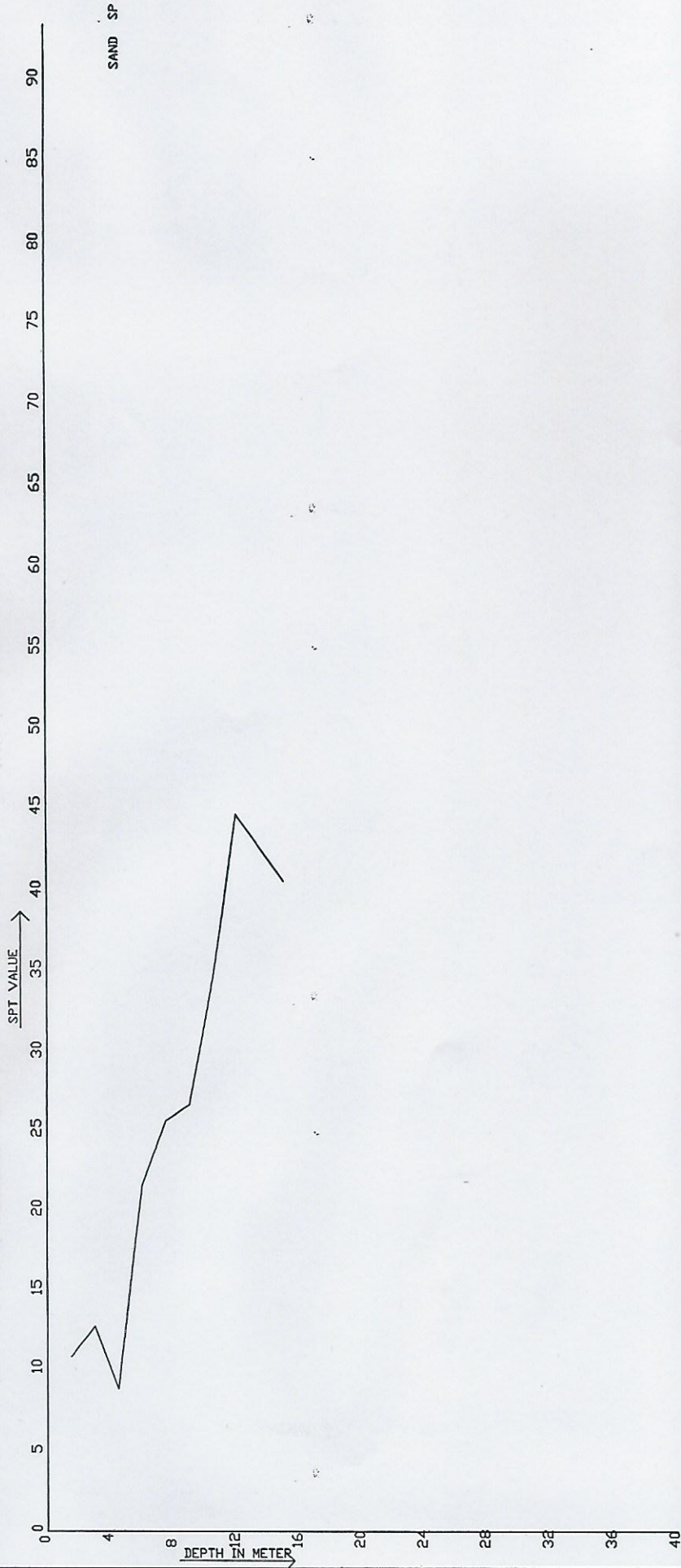
TRIAxIAL/DIRECT TEST RESULT



BORE LOG AND DEPTH ~ SPT GRAPH (CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA.)

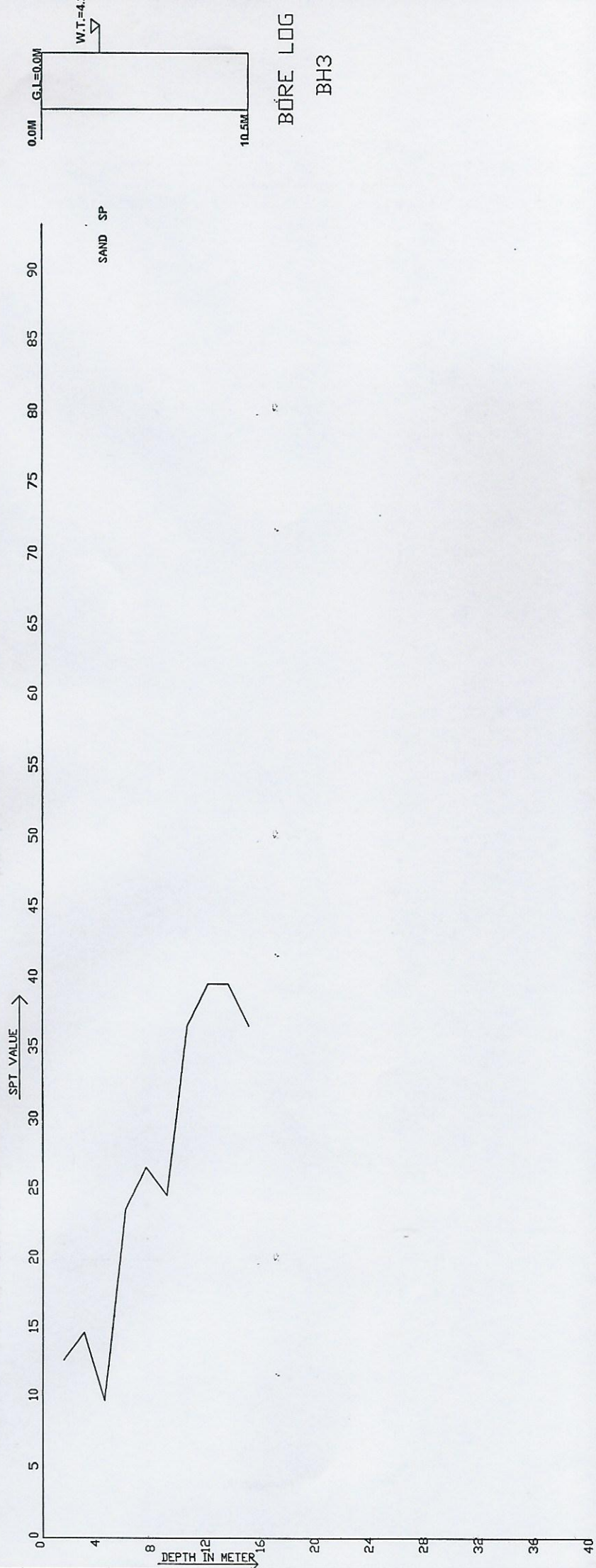


BORE LOG AND DEPTH ~ SPT GRAPH (CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA.)

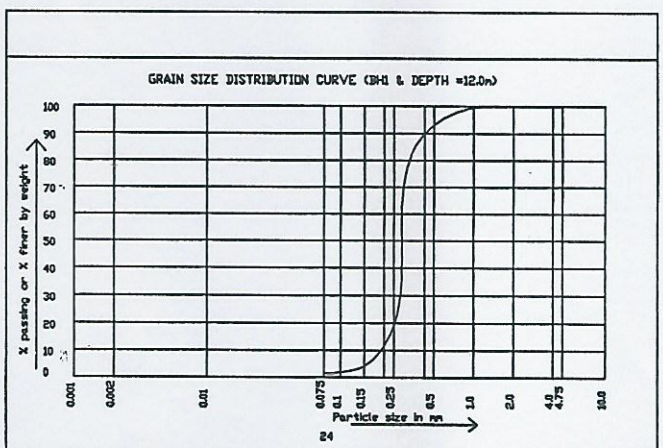
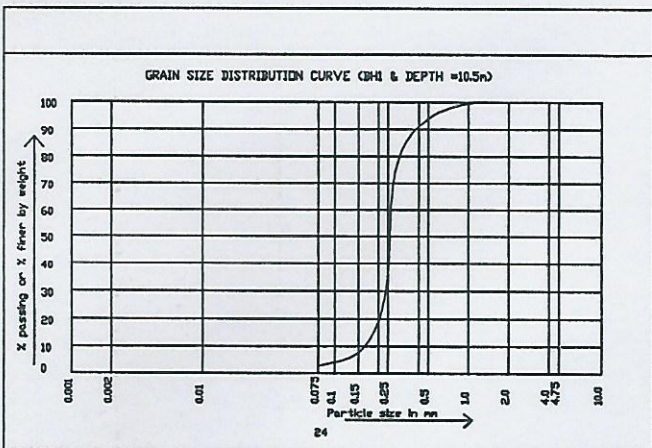
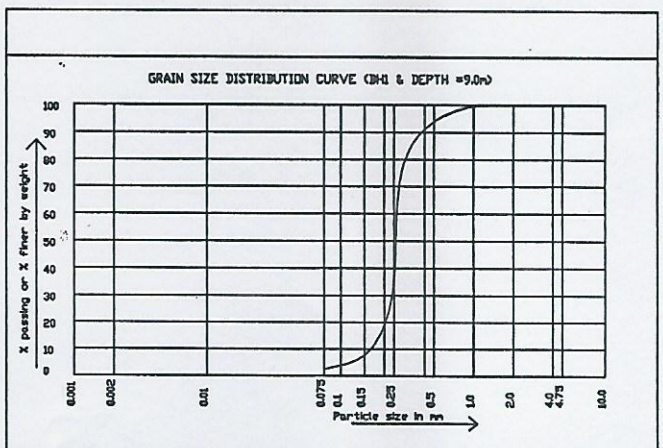
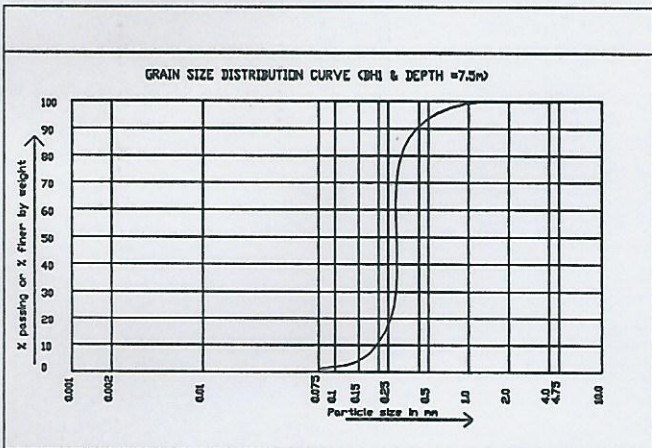
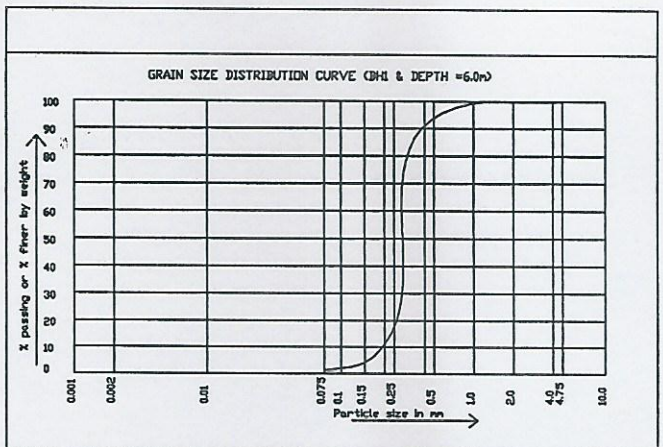
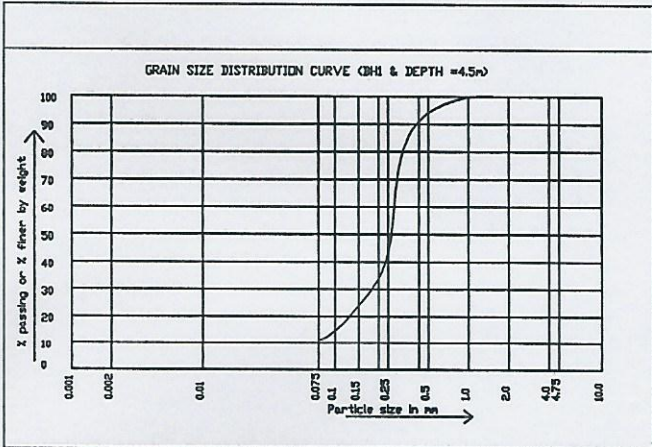
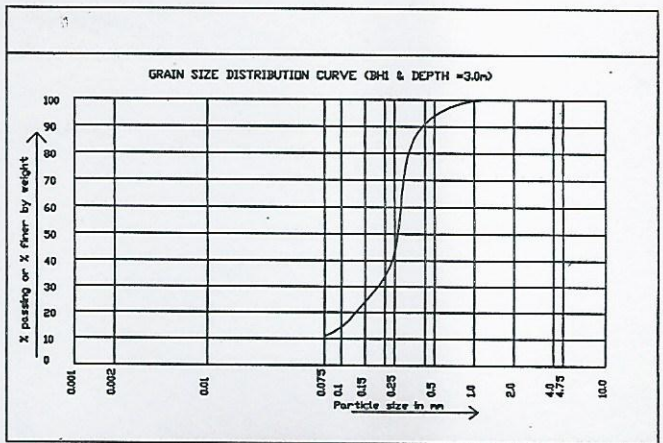
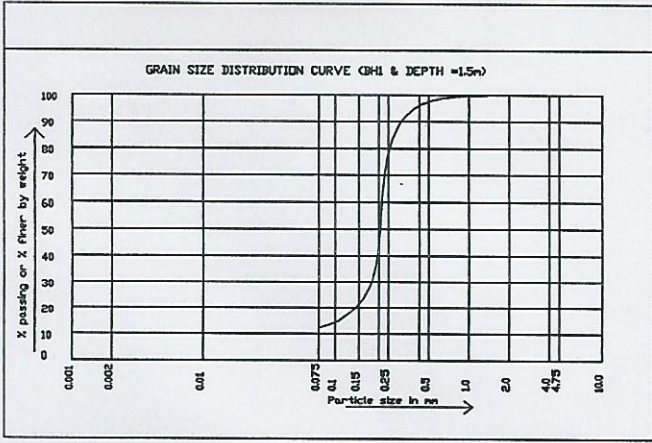


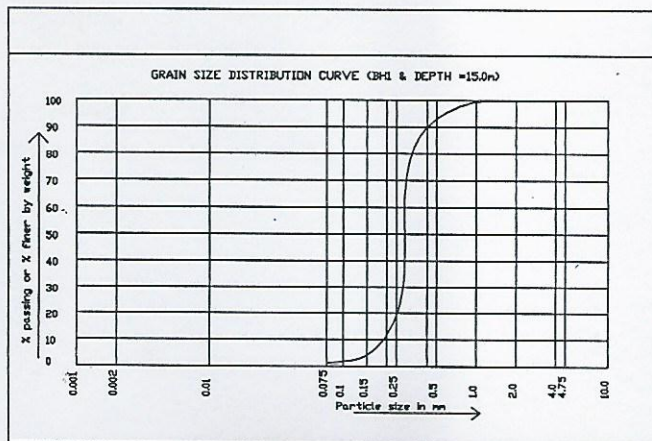
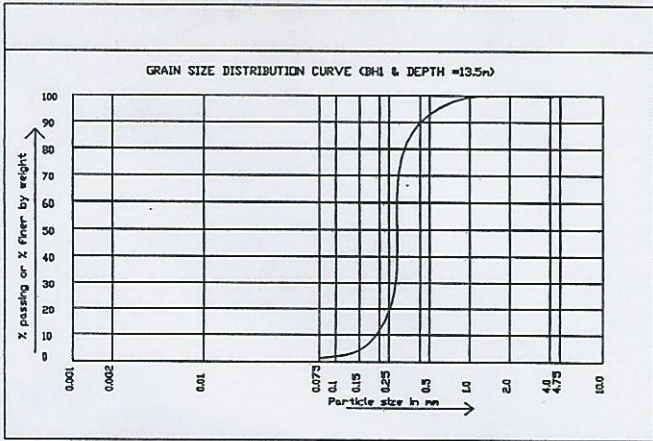
BORE LOG
BH2

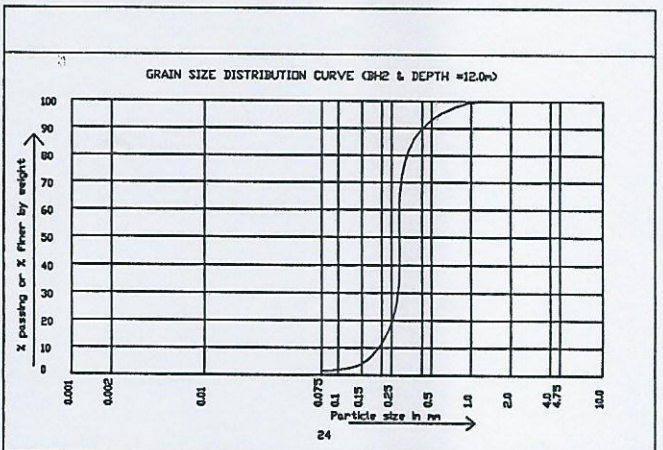
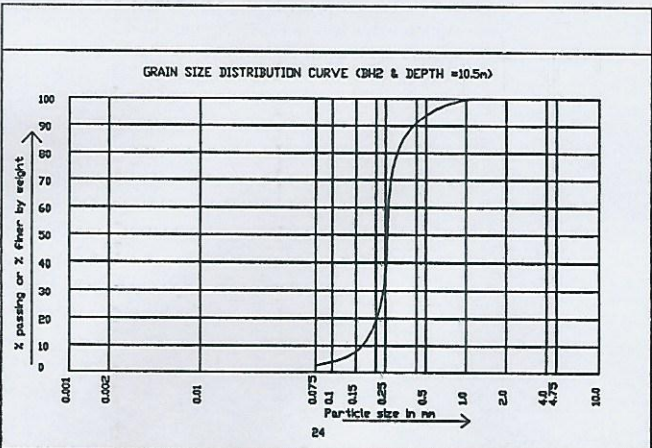
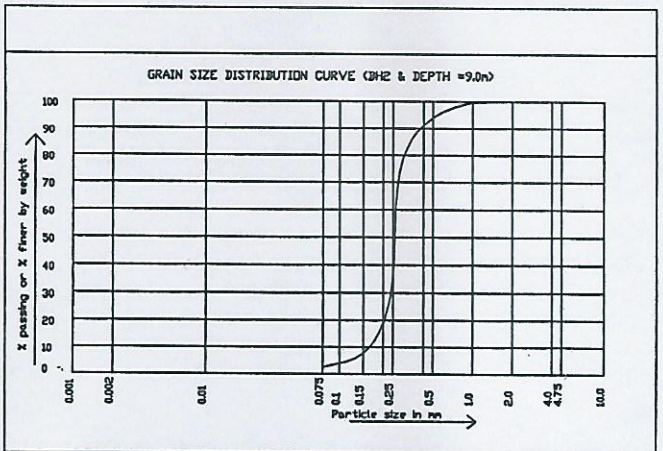
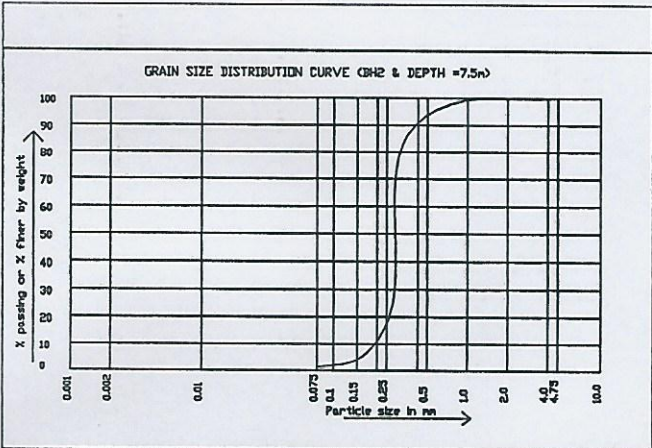
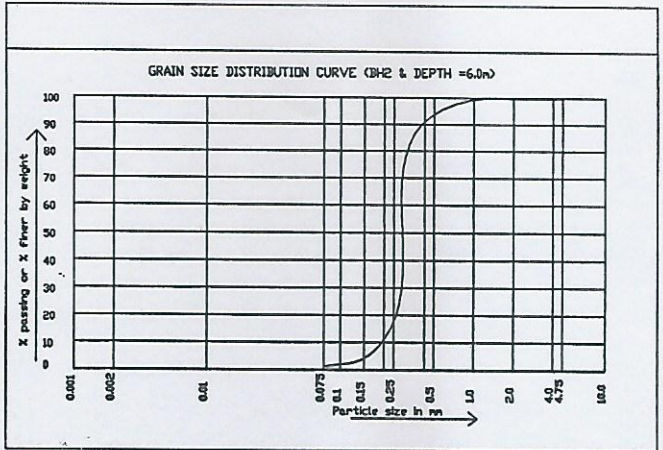
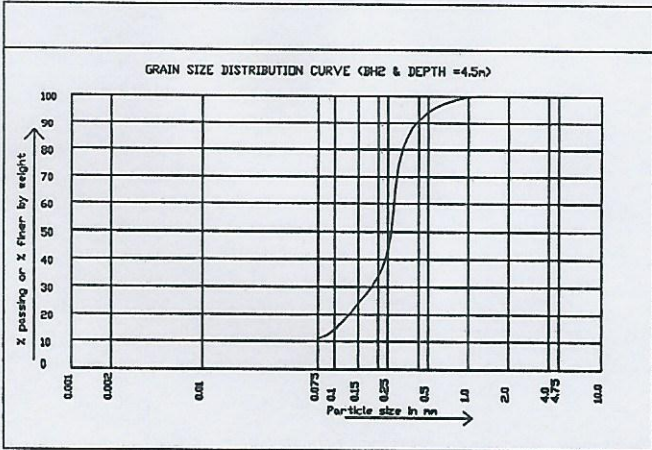
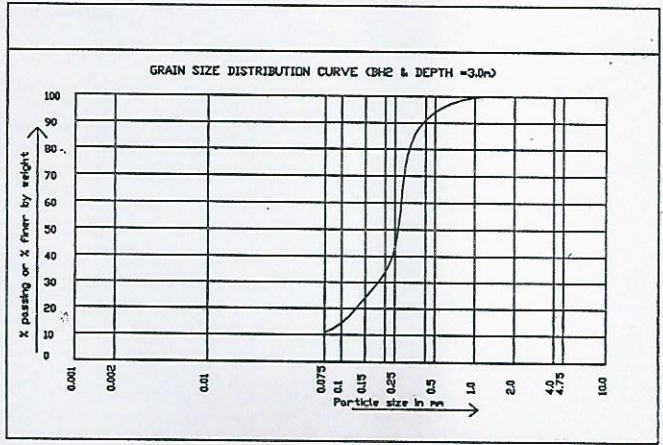
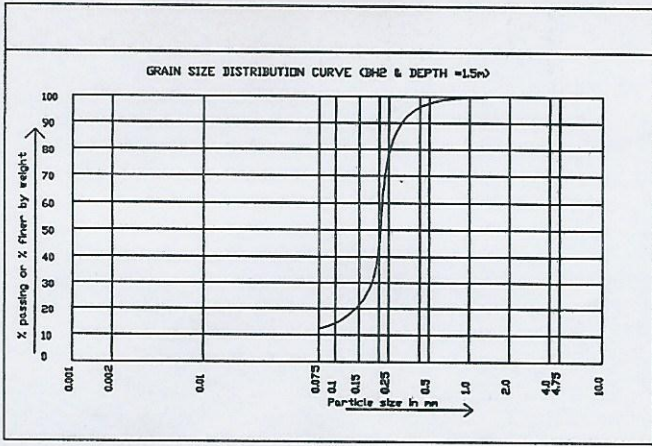
BORE LOG AND DEPTH ~ SPT GRAPH (CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA)

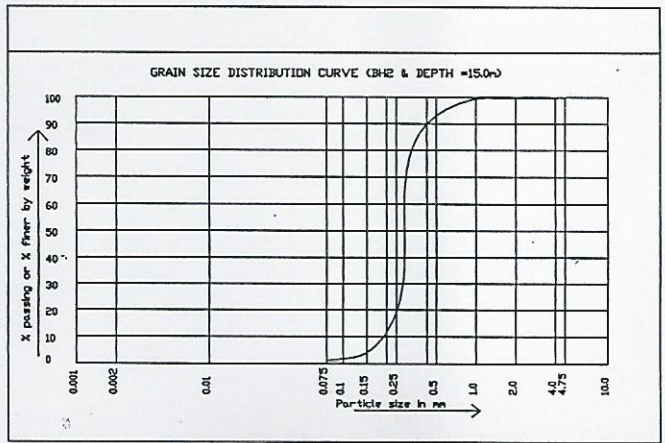
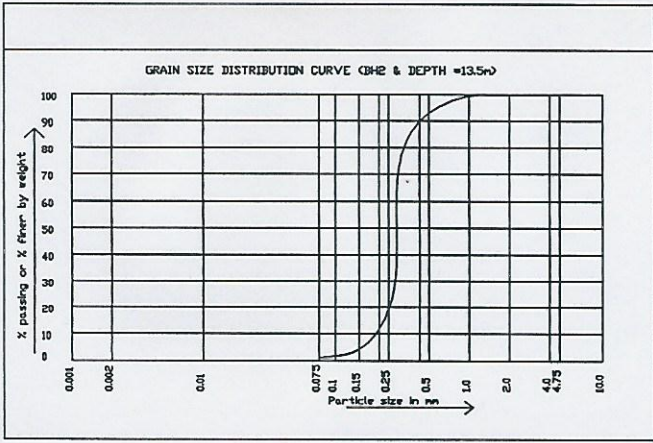


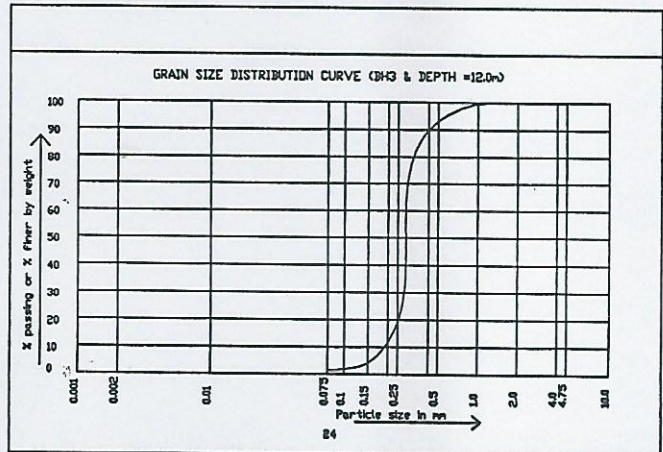
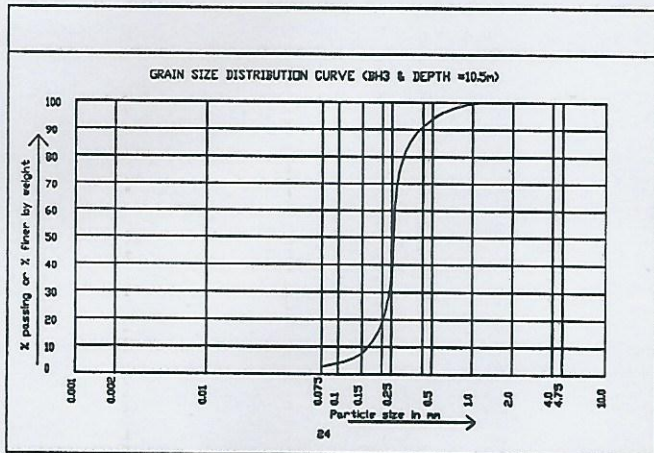
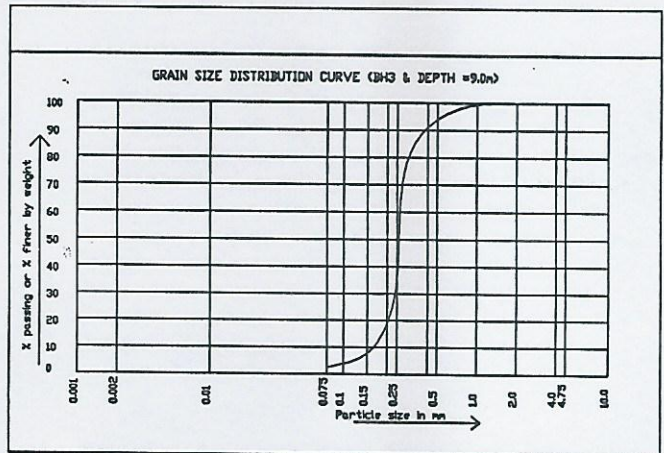
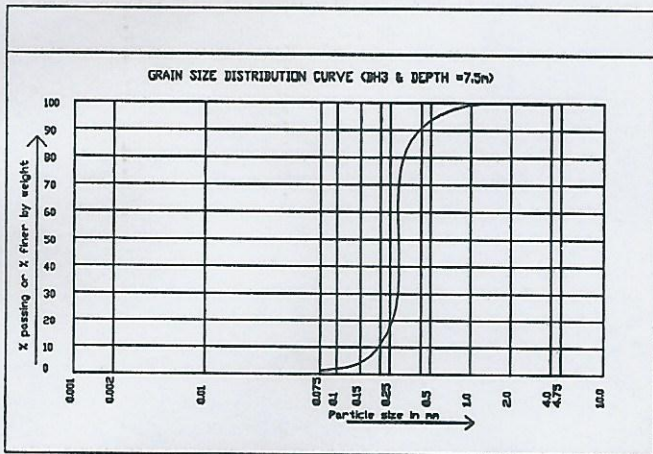
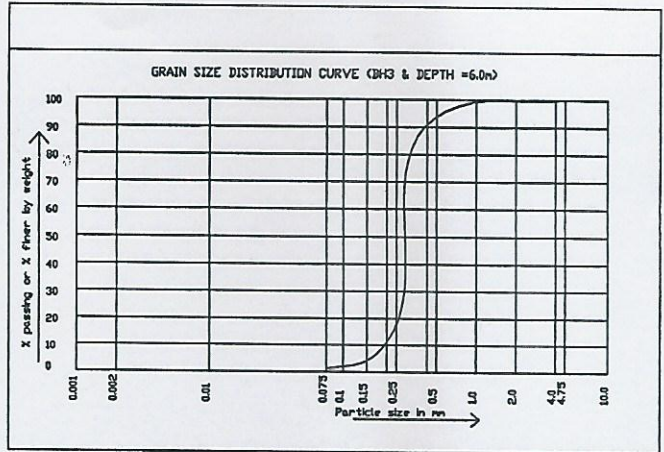
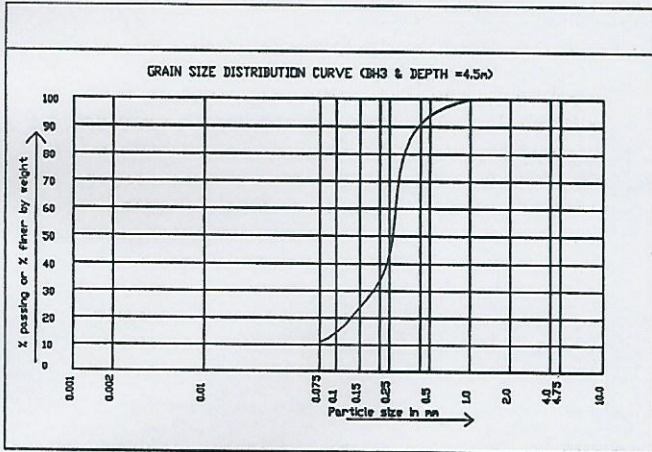
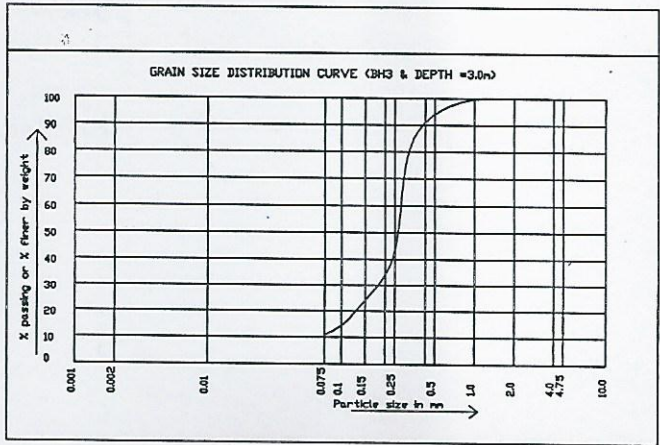
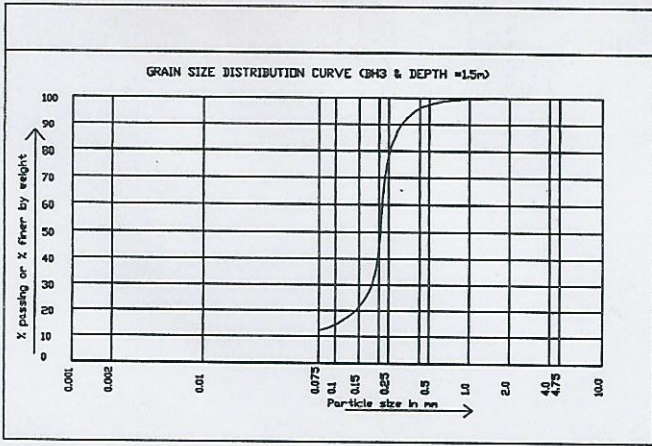
BORE LOG
BH3

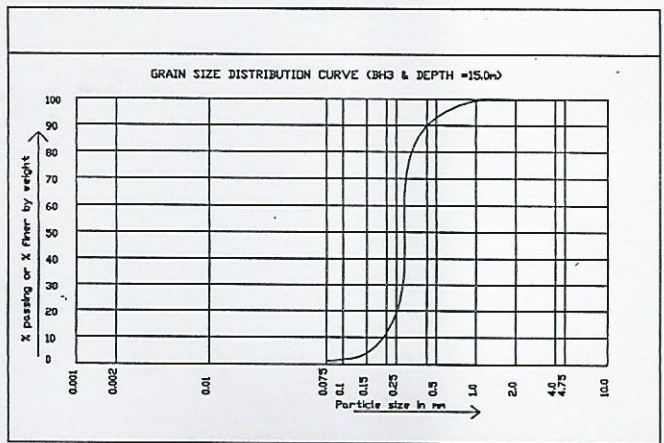
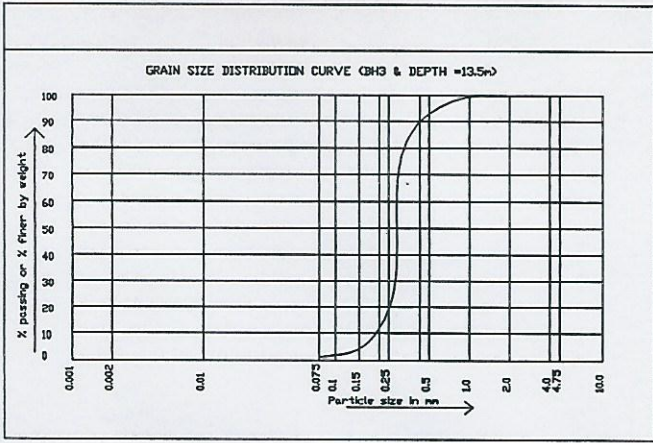












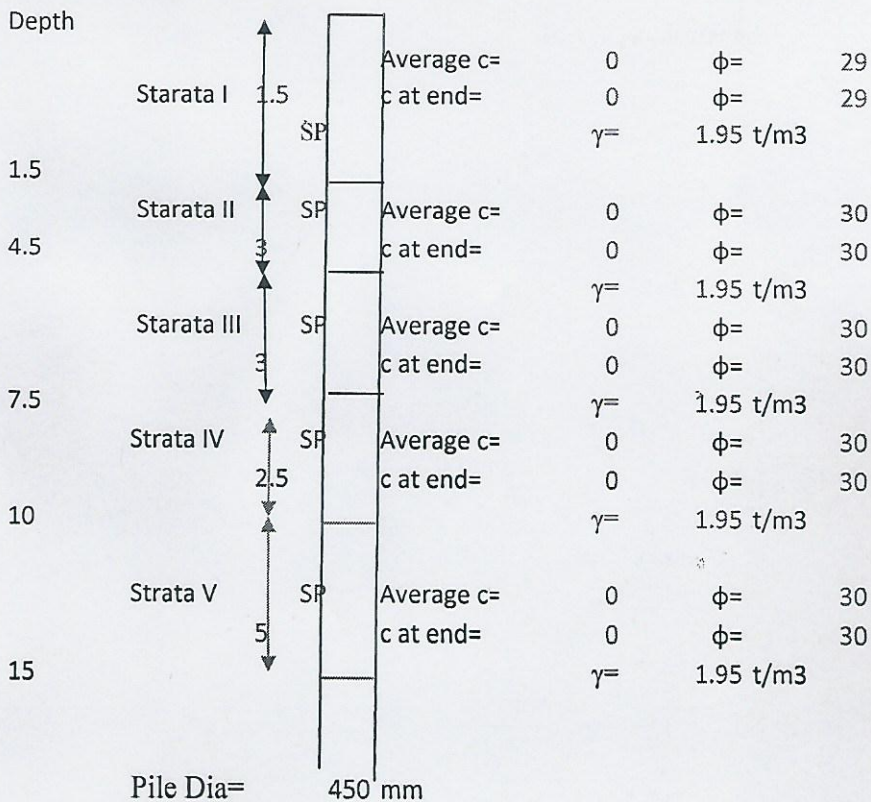
Calculation of Net safe Bearing Capacity for Strip Footing

Table 1 BEARING CAPACITY FACTORS AS PER IS 6403 : 1981

Angle of shearing resistance of soil, phi	Nc	Nq	Ny						
0	5.14	1	0						
5	6.49	1.57	0.45						
10	8.35	2.47	1.22						
15	10.98	3.94	2.65						
20	14.83	6.4	5.39						
25	20.72	10.66	10.88						
30	30.14	18.4	22.4						
35	46.12	33.3	48.03						
40	75.31	64.2	109.41						
45	138.88	134.88	271.76						
50	266.89	319.07	762.89						
Depth of footing below GL in meter D=	1.5								
Width of footing in meter, B=	2			Water Table considered=		1.5 m below GL			
Effective depth of soil formation contributing in	2.83								
Average cohesion of soil mobilised in Ton/m2=	0.00								
unit weight of soil in ton/m2, γ=	1.94								
Angle of shearing resistance of soil, phi, in degree =	29.00		Corresponding Nc/N'c=	15.27	Corresponding Nq/N'q=	6.72	Corresponding Ny/N'y=	5.80	
Effective Angle of shearing resistance of soil, phi, in degree =	20.37		Corresponding Nc/N'c=	15.27	Corresponding Nq/N'q=	6.72	Corresponding Ny/N'y=	5.80	
Depth factor, dc=	1.22	$dc=1+0.2*(Df/B)*\tan(45+\phi/2)$							
Depth factor, dq=	1.11	$dq=1+0.1*(Df/B)*\tan(45+\phi/2)$ if $\phi > 10$ otherwise $dq=1$							
Depth factor, dy=	1.11	$dy=1+0.1*(Df/B)*\tan(45+\phi/2)$ if $\phi > 10$ otherwise $dy=1$							
effective surcharge at base level of foundation, q=yD	2.9	q=yD							
Q1 ton/m2 =	0.00	$Q1=(2/3)*c*N'c*dc$							
Q2 ton/m2 =	18.413	$Q2=q*(N'q-1)*dq$							
Q3 ton/m2 =	6.05	$Q3=(1/2)*B*\gamma*N'y*dy*W'$							
ultimate bearing capacity Q ton/m2 =	24.46	$Q=Q1+Q2+Q3$							
Factor of safety, F.S. =	3								
Net Safe Bearing Capacity in ton/m2 q=	8.15	$q=Q1/F.S.$							

Calculation of Net safe Bearing Capacity for Isolated Square/Rectangular Footing										
Footing size	Length L in meter	Width B in meter								
	2	2								
Shape factors	Sc	Sq	Sy							
	1.3	1.2	0.8							
Q1 ton/m2 =	0.00	Q1=(2/3)*c*Nc*dc*S								
Q2 ton/m2 =	22.10	Q2=q*(Nq-1)*dq*Sq								
Q3 ton/m2 =	4.84	Q3=(1/2)*B*y*Ny*dy *Sy*W								
ultimate bearing capacity Q ton/m2 =	26.94	Q=Q1+Q2+Q3								
Factor of safety, F.S. =	3									
Net Safe Bearing Capacity in ton/m2 q=	8.98	q=Q1/F.S.								

Pile Design



Pile Dia= 450 mm

A_p = base area= 0.159 m²

Overburden Pressure corresponding to L(6.75m) = 6.4125 t/m²

Strata I

φ	N _c	N _q	N _y	Average c at end	α	γ
29	28.26	16.850	20.10	0	1.00	1.95

Top of Strata
 Depth= 0.000
 Pressure= 0.000 due to submerged soil
 Average γ= 1.95 t/m³

Effective length for overburden estimation=(15x0.45m)= 6.75 m
 Pressure(Limiting at top of Strata)= 6.410 t/m²

End of Strata
 Overburden Pressure corresponding to L(15x0.45m)=6.75m 6.41 t/m²
 Depth= 1.500 Average γ= 1.95 t/m³
 Pressure= 1.425 t/m² due to submerged soil
 Pressure at end of strata= 1.425 not greater than limiting

Average Pressure in Strata for end bearing= 3.9175 t/m²
 Average Pressure in Strata for skin bearing= 3.9175 t/m²
 Surface area of Starata I= 2.121 m²

Capacity due to fine grained soil

$Q_{skin} = \lambda \alpha c A_s = 0.0 \text{ t}$

$Q_{end} = A_p N_c C_p = 0.0 \text{ t}$

Capacity due to coarse grained soil

$k = 1 \quad \delta = 29 \quad N_q = 18$

Skin friction in ton $Q_s = k \cdot P_d \cdot \tan(\delta) \cdot A_s = 1 \times 3.9175 \times \tan(\pi \times 29 / 180) \times 2.121 = 4.6 \text{ t}$

End bearing in ton $Q_b = A_p \cdot [0.5 \cdot D \cdot \gamma \cdot N_y + P_d \cdot N_q] = 0.159 \times (0.5 \times 0.45) \times (1.95 - 1) \times 20.1 + 1.425 \times 18 = 4.8 \text{ t}$

ϕ	30	40	For $\phi=29$ Degree
K	1	1.5	1
Critical Depth factor	15	20	15.0

Strata II

ϕ	Nc	Nq	Ny	Average c= c at end	α	γ
30	30.14	18.400	22.40	0	1.00	1.95

Top of Strata

Depth= 1.500 Average γ = 1.95 t/m3
 Pressure= 1.425 due to submerged soil
 Effective length for overburden estimation=(15x0.45m)= 6.75 m
 Pressure(Limiting at top of Strata)= 1.425 t/m2
 End of Strata
 Overburden Pressure corresponding to L(15x0.45m)=6.75m 6.41 t/m2
 Depth= 4.500 Average γ = 1.95 t/m3
 Pressure= 4.275 t/m2 due to submerged soil
 Pressure at end of strata= 4.275 not greater than limiting
 Average Pressure in Strata for end bearing= 2.850 t/m2
 Average Pressure in Strata for skin bearing= 2.85 t/m2
 Surface area of Strata II= 4.241 m2

Capacity due to fine grained soil

$Q_{skin} = \alpha c A_s = 0.0 \text{ t}$

$Q_{end} = A_p N_c C_p = 0.0 \text{ t}$

ϕ	30	40	For $\phi=30$ Degree
K	1	1.5	1
Critical Depth factor	15	20	15.0

Capacity due to coarse grained soil

$k=1$ $\delta=30$ $N_q=20$
 Skin friction in ton $Q_s = k \cdot P_d \cdot \tan(\delta) \cdot A_s =$
 $= 1 \times 2.85 \times \tan(\pi \times 30 / 180) \times 4.241 = 6.98 \text{ t}$
 End bearing in ton $= Q_b = A_p \cdot [0.5 \cdot D \cdot \gamma \cdot N_y + P_d \cdot N_q] =$
 $= 0.159 \times (0.5 \times (0.45) \times (1.95 - 1) \times 22.4 + 4.275 \times 20) = 14.4 \text{ t}$

Strata III

ϕ	Nc	Nq	Ny	Average c= c at end	α	γ
30	30.14	18.400	22.40	0	1.00	1.95

Top of Strata

Depth= 4.500 Average γ = 1.95 t/m3
 Pressure= 4.275 due to submerged soil
 Effective length for overburden estimation=(15x0.45m)= 6.75 m
 Pressure(Limiting at top of Strata)= 4.275 t/m2
 End of Strata
 Overburden Pressure corresponding to L(15x0.45m)=6.75m 6.41 t/m2

Depth= 7.500 Average γ = 1.95 t/m³
 Pressure= 7.125 t/m² due to submerged soil
 Pressure at end of strata= 6.410 not greater than limiting
 Average Pressure in Strata for end bearing= 5.3425 t/m²
 Average Pressure in Strata for skin bearing= 5.70
 Surface area of Strata III= 4.241 m²

Capacity due to fine grained soil

Q skin= $\xi \alpha c A_s$ = 0.000 t

Q end= $A_p N_c C_p$ = 0.000 t

			For $\phi=30$
ϕ	30	40	Degree
K	1	1.5	1
Critical Depth factor	15	20	15.0

Capacity due to coarse grained soil

k= 1 delta= 30 Nq = 20

Skin friction in ton $Q_s = k \cdot P_d \cdot \tan(\delta) \cdot A_s =$
 $= 1 \times 5.7 \times \tan(\pi \times 30 / 180) \times 4.241 =$ 13.957 t

End bearing in ton $Q_b = A_p \cdot [0.5 \cdot D \cdot \gamma \cdot N_y + P_d \cdot N_q] =$
 $= 0.159 \times (0.5 \times (1.95 - 1) \times 22.4 + 6.41 \times 20) =$ 21.145 t

Strata IV

ϕ	Nc	Nq	Ny	Average c= c=	c at end	α	γ
30	30.14	18.400	22.40	0	0	1.00	1.95

Top of Strata

Depth= 7.500 Average γ = 1.95 t/m3

Pressure= 7.125 due to submerged soil

Effective length for overburden estimation=(15x0.45m)= 6.75 m

Pressure(Limiting at top of Strata)= 6.410 t/m2

End of Strata

Overburden Pressure corresponding to L(15x0.45m)=6.75m 6.41 t/m2

Depth= 10.000 Average γ = 1.95 t/m3

Pressure= 9.500 t/m2 due to submerged soil

Pressure at end of strata= 6.410 not grater than limiting

Average Pressure in Strata for end bearing= 6.41 t/m2

Average Pressure in Strata for skin bearing= 6.41

Surface area of Starata IV= 3.534 m2

Capacity due to fine grained soil

Q skin= $\sum \alpha c A_s = 0.000$ t

	30	40	For $\phi=30$ Degree
K	1	1.5	1
Critical Depth factor	15	20	15.0

Q end= $A_p N_c C_p = 0.000$ t

Capacity due to coarse grained soil

k= 1 delta= 30 Nq = 20

Skin friction in ton $Q_s = k * P_d * \tan(\delta) * A_s = 1 * 6.41 * \tan(\pi * 30 / 180) * 3.534 = 13.079$ t

End bearing in ton $= Q_b = A_p * [0.5 * D * \gamma * N_y + P_d * N_q] = 0.159 * (0.5 * (0.45) * (1.95 - 1) * 22.40 + 6.41 * 18.400) = 21.145$ t

Strata V

ϕ	Nc	Nq	Ny	c=	c at end	α	γ
30	30.14	18.400	22.40	0	0	1.00	1.95

Top of Strata

Depth= 10.000 Average γ = 1.95 t/m3

Pressure= 9.500 due to submerged soil

Effective length for overburden estimation=(15x0.45m)= 6.75 m

Pressure(Limiting at top of Strata)= 6.410 t/m2

End of Strata

Overburden Pressure corresponding to L(15x0.45m)=6.75m 6.41 t/m2

Depth= 15.000 Average γ = 1.95 t/m3

Pressure= 14.250 t/m2 due to submerged soil

Pressure at end of strata= 6.410 not grater than limiting

Average Pressure in Strata for end bearing= 6.41 t/m2

Average Pressure in Strata for skin bearing= 6.41

Surface area of Starata IV= 7.069 m2

Capacity due to fine grained soil

$Q_{skin} = \lambda \alpha c A_s = 0.000 \text{ t}$

$Q_{end} = A_p N_c C_p = 0.000 \text{ t}$

Capacity due to coarse grained soil

$k = 1 \quad \delta = 30 \quad N_q = 20$

Skin friction in ton $Q_s = k \cdot P_d \cdot \tan(\delta) \cdot A_s = 1 \times 6.41 \times \text{TAN}(\pi \times 30/180) \times 7.069 = 26.161 \text{ t}$

End bearing in ton $= Q_b = A_p \cdot [0.5 \cdot D^* \cdot y \cdot N_y + P_d \cdot N_q] = 0.159 \times (0.5 \times 0.45) \times (1.95 - 1) \times 22.4 + 6.41 \times 20 = 21.145 \text{ t}$

			For $\phi=30$
ϕ	30	40	Degree
K	1	1.5	1
Critical Depth factor	15	20	15.0

Capacity of Pile

Dia= 450 mm

Depth= 10.000 M

Capacity= (4.6)+(6.98) + (13.957)+(34.224)= 59.76 t

F.S.= 2.500

Safe Capacity= 23.9 t

CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA

Table 11

Soil stratification

DEPTH	SOIL TYPE	CONSISTANCY	CLASSIFICATION
0.0-10.5	SAND	MEDIUM TO DENSE	SP

WATER TABLE was found at the depth of about 4.2m below GL as reported May'2023.

RECOMMENDATION

The present report is prepared on the basis of lab. Test result & field test conducted in the field.

The lab. test result is obtained by conducting different test on representative sample obtained through 3 no. of bore holes whose location and depth were decided by BSEIDC and shown in the bore hole location plan.

The laboratory test of soil samples obtained in all bore holes are given in Tables 2-10. Study of these tables reveals that the sub-soil strata :

- (a) Soil strata consist of coarse grained soil.

Therefore, foundation should be placed at 1.50m or beyond the ground level. Both, shallow as well as deep, foundations are feasible. Plane piles are feasible BUT, it is difficult to place the pile in sand.

By way of example the calculated value of safe capacity of certain type and size of Shallow foundation are being tabulated below: -

STRIP FOOTING

Depth below GL (m)	Width of foundation (m)	Safe Bearing capacity (t/m ²)	Maximum expected settlement(mm)	Bearing capacity(t/m ²) against maximum settelement	Allowable Bearing capacity(t/m ²)
1.5	2.0	8.0	50	10	8
	3.0	8.5	50	9.0	8.5

SQUARE FOOTING

Depth below GL (m)	Foundation size (m)	Safe Bearing capacity (t/m ²)	Maximum expected settlement(mm)	Bearing capacity(t/m ²) against maximum settelement	Allowable Bearing capacity(t/m ²)
1.5	2 X2	8.5	50	11	8.5

CONSTRUCTION OF SHIKSHA BHAWAN (G+4) AT MADHEPURA

By way of example the calculated value of safe capacity of certain diameter of piles using IS : 2911 (Part 1/Sec 2) 2010:

Plane Pile Capacity

Depth of Pile below GL(m)	Dia of Pile (m)	Allowable Capacity (Ton)
10	0.45	20
10	0.6	35

Limitation

If the sub-soil condition is found much different from those reported here during trenching, suitable steps should be taken. Back filling over footing shall be done with proper compaction.

Pile capacity shall be confirmed by Initial and Routine pile load test as per relevant Indian codes. Group efficiency shall be considered for group of pile.

Anil Kumar Sariaar

ANIL KUMAR SARIAR
Partner, Shamvvi consultant